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# Ultrasonic degradation of poly (styrene-*co*-alkyl methacrylate) copolymers

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# **ABSTRACT**

The ultrasonic degradation of poly (styrene-*co*-methyl methacrylate) (SMMA), poly (styrene-*co*-ethyl methacrylate) (SEMA) and poly (styrene-*co*-butyl methacrylate) (SBMA) copolymers of different compositions was studied. The copolymers were synthesized and NMR spectroscopy was used to determine the composition, and the glass transition temperatures were determined by DSC. The reactivity ratios were determined by the Kelen–Tudos method and it indicated that the copolymers were random. The effect of solvent, temperature and copolymer composition on the ultrasonic degradation rate of these copolymers was investigated. A model based on continuous distribution kinetics was employed to study the degradation kinetics. The degradation rate coefficients of the copolymers decreased with an increase in the styrene content in the copolymer. At any particular copolymer composition the rate of degradation follows the order: SBMA > SEMA > SMMA. Thermogravimetric analysis (TGA) of the copolymers was carried in order to assess their thermal stability. The same order of degradation was observed for the thermal degradation of the copolymers as that observed for ultrasonic degradation.

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#### 1. Introduction

The copolymers of styrene and alkyl methacrylates represent a widely-used class of copolymers since they exhibit great diversity of properties compared to those of homopolymers [\[1\]](#page-6-0). Their high thermal and chemical stability, high transparency, easy formability, good electrical and mechanical properties [\[2\]](#page-6-0) has led them to be used for a variety of applications in medicine, paper and paint industry, textiles and automobiles etc. For example, solid polystyrene is used in disposable cutlery, plastic models, CD and DVD cases, and the expanded form of polystyrene is used for packing materials and insulation [\[3\].](#page-6-0) Poly(alkyl methacrylates) are mainly used in intraocular lenses, control drug delivery systems and adhesives, respectively. The copolymers of styrene and alkyl methacrylates are used in gamma irradiation shields, plastic optical fibers and synthetic resins [\[3\]](#page-6-0).

The common method of degradation is by the use of thermal or chemical energy. Among the alternative methods of polymer degradation, ultrasonic degradation is interesting because unlike chemical and thermal degradation methods, ultrasonic degradation occurs by non-random mid point scission [\[4\].](#page-6-0) The overall degradation mechanism of polymer molecules in presence of ultrasound is primarily by the action of intense shear fields set up by the collapsing cavities of microbubbles [\[5\].](#page-6-0) The influence of various factors such as solvent, temperature, ultrasound intensity [\[6\],](#page-6-0) polymer concentration [\[4\]](#page-6-0), initial molecular weight [\[7\],](#page-6-0)

dissolved gases [\[8\]](#page-6-0), viscosity and surface tension [\[9,10\]](#page-6-0) affecting the degradation of different polymer solution systems has been investigated in various studies.

Many theoretical [\[11–13\]](#page-6-0) and phenomenological models [\[14–](#page-6-0) [16\]](#page-6-0) have been proposed by several researchers to evaluate the kinetics of the ultrasonic degradation process. All of these models offer the same rough description of the reduction of the average molecular weight during the process [\[17\].](#page-6-0) All the models show that the polymer degrades rapidly in the initial phase of the process, and then the rate of decrease of molecular weight slows down and approaches a limiting molecular weight. Continuous distribution kinetic models [\[7,9,18\]](#page-6-0) have been successfully used to determine the degradation rate coefficient and the same approach has been followed in this study.

The ultrasonic degradation of polystyrene [\[8,19\],](#page-6-0) poly(methyl methacrylate) [\[20\]](#page-6-0), poly(vinyl-pyrrolidone) [\[21\],](#page-6-0) poly(ethylene oxide) [\[22,23\],](#page-6-0) poly(vinyl acetate) [\[4,24\],](#page-6-0) polyvinyl alcohol [\[25\],](#page-6-0) poly(alkyl methacrylates) [\[26\]](#page-6-0) has been studied. The ultrasonic degradation of poly(methyl methacrylates-*co*-alkyl acrylate) copolymers was investigated [\[27\]](#page-6-0) and it was shown that the degradation rate varies linearly with the alkyl acrylate content in the copolymer. However, ultrasonic degradation of copolymers and the effect of copolymer composition on the degradation rate have not been well studied.

In this work, poly (styrene-*co*-alkyl methacrylates) copolymers, viz. poly (styrene-*co*-methyl methacrylate) (SMMA), poly (styrene*co*-ethyl methacrylate) (SEMA) and poly (styrene-*co*-butyl methacrylate) (SBMA) over the entire range of composition were prepared and the kinetics of the ultrasonic degradation was studied. To the



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<span id="page-1-0"></span>best of our knowledge, this is the first study on the ultrasonic degradation of poly (styrene-*co*-alkyl methacrylate) copolymers. The main objective of our study was to investigate the effect of copolymer composition and alkyl group substituent on the ultrasonic degradation and compare the trend with the thermal stability of these copolymers.

# 2. Experimental

# *2.1. Materials and methods*

The monomers, styrene, methyl methacrylate, ethyl methacrylate and butyl methacrylate were procured from Sigma–Aldrich (USA) and washed with 5% caustic solution in order to remove inhibitors. This was followed by distillation under pressure to ensure the purity of monomers. The solvents, benzene, chlorobenzene, *o*-dichlorobenzene, toluene, and *p*-xylene; and the initiator, azo-bis-isobutyronitrile (AIBN) were purchased from S.D. fine chemicals (India). The solvents were distilled and filtered through  $0.2 \mu$ m nylon filter paper before use.

# *2.2. Polymerization*

All polymers were synthesized by using conventional free radical polymerization technique using AIBN (5% wt.) as the initiator at 60  $\degree$ C. The synthesized polymers were fractionated by dissolving in toluene and subsequent precipitation in methanol.

#### *2.3. Ultrasonic degradation experiments*

Polymer solutions of 2 g/L were prepared and 60 mL of the polymer solution was subjected to ultrasonic degradation using a horntype ultrasonic processer (Vibronics, India) with an intensity of 36 W/cm<sup>2</sup> . SMMA-54 (styrene–methyl methacrylate copolymer with 54 mol% of methyl methacrylate) was degraded in different solvents at 30 $\degree$ C to understand the effect of solvents and was also degraded at different temperatures from 30 to 60 °C in *o*-dichlorobenzene. The temperature of the solution was maintained constant  $(\pm 2 \degree C)$  using a thermostatic water bath. The homopolymers and copolymers of different compositions were degraded in *o*-dichlorobenzene at 30 $\degree$ C. Further details of the experimental setup can be found elsewhere  $[27]$ . Samples of 200  $\mu$ L were collected for further analysis by gel permeation chromatography (GPC). To obtain the limiting molecular weight of the polymers, experiments were carried for 10 h and no significant change was observed in molecular weight after 8 h. Several experiments were repeated in triplicate and the error in estimation of rate coefficient was less than 4%.

## *2.4. GPC analysis*

The molecular weight (MW) distributions of the samples were determined by GPC that consisted of a high pressure liquid chromatography (HPLC) pump, three size exclusion columns packed with cross linked poly (styrene-divinyl benzene) (Styragel HR 5E, HR 4, HR 1)  $[300 \text{ mm} \times 7.5 \text{ mm}]$ , a differential refractometer



Fig. 1. Ozawa plots to determine activation energies of homo polymers (a) PBMA, (b) PEMA, (c) PMMA and (d) PS. The numbers on the plot indicate conversion.

<span id="page-2-0"></span>(Waters RI 2410) for detection, and a data acquisition system to store the data. The samples were injected through a Rheodyne 7725i valve with a sample loop of 50 uL. The obtained chromatogram was converted to molecular weight distribution (MWD) using universal calibration [\[28\]](#page-6-0). Tetrahydrofuran (THF) was used as the eluent at a flow rate of 1 mL/min.

# *2.5. NMR characterization*

 $1$ H NMR (400 MHz, Bruker) spectroscopy was used to determine the compositions of the synthesized copolymers, using  $CDCl<sub>3</sub>$  as solvent and tetramethysilane (TMS) as reference.

# *2.6. TGA analysis*

All the homo polymers and copolymers (10–15 mg) were subjected to pyrolysis using the Perkin–Elmer Pyris-Diamond thermogravimetric-differential thermal analyzer (TG/DTA) in an inert atmosphere (nitrogen flow at 150 cm<sup>3</sup>/min) at different heating rates (5–20 °C/min) in the temperature range of 30–700 °C.

# *2.7. DSC analysis*

The calorimetric (DSC) measurements were carried out on a DSC823<sup>e</sup> differential scanning calorimeter (Mettler Toledo, US)

operating in a nitrogen atmosphere. The sample size was around 20 mg. The analysis was performed at the heating rate of  $5 \degree C/min$ .

# 3. Theoretical model

Continuous distribution kinetics was used in this study to determine the degradation rate coefficients [\[27\].](#page-6-0) For a polymer  $P(x)$ , the ultrasonic midpoint degradation can be represented as follows [\[28\]](#page-6-0)

$$
P(x) \stackrel{k(x)}{\rightarrow} 2P(x/2) \tag{1}
$$

The population balance equation for the above equation can be written as [\[7\]](#page-6-0)

$$
\frac{\partial p(x,t)}{\partial t} = -\kappa(x)p(x,t) + 2\int_x^\infty \kappa(x')p(x',t)\delta\left(x - \frac{x'}{2}\right)dx'
$$
 (2)

The degradation rate coefficient is assumed to be of the form  $\kappa$  $(x)$  =  $k(x - x_l)$ , where  $x_l$  is the limiting molecular weight [\[23\].](#page-6-0) This form of the rate equation indicates that no further degradation is possible after the polymer reaches its limiting molecular weight. Applying the moment operation and solving the moment equations yields the variation of the number average molecular weight (*Mn*) as [\[27\]](#page-6-0)

$$
\ln\left(\frac{\frac{1}{M_{n0}}-\frac{1}{x_l}}{\frac{1}{M_n}-\frac{1}{x_l}}\right)=\ln(Y)=kx_l t
$$
\n(3)



Fig. 2. Ozawa plots to determine activation energies of (a) SMMA-54, (b) SEMA-56 and (c) PBMA-54 copolymers.

# <span id="page-3-0"></span>4. Results and discussion

#### *4.1. Copolymer composition*

All copolymers were analyzed using 400 MHz $<sup>1</sup>$ H NMR spectros-</sup> copy, and the compositions of the copolymers were calculated by identifying and quantifying the signal peaks of the monomers. The <sup>1</sup>H NMR spectrum of SMMA-54 (54 mol% methyl methacrylate) copolymer is shown in Fig. S1 (see supplementary information). It is reported that styrene shows a peak at  $\delta$  = 7.1 [\[29,30\]](#page-6-0) and MMA at  $\delta$  = 2.8–3.6 [\[30,31\]](#page-6-0) corresponding to the phenyl ring  $(-C_6H_5)$  and the methoxy ester linkage  $(-COOCH_3)$ , respectively. These peaks were identified in all copolymers and compositions of the copolymers were calculated from the integral peak areas [\[29,31\].](#page-6-0) Similarly the compositions of SEMA and SBMA copolymers were computed from integrating the signal peak areas of EMA at  $\delta$  = 3.8 [\[32,33\]](#page-6-0) and of BMA at  $\delta$  = 4.2 [\[32–34\].](#page-6-0)

The Kelen–Tudos method [\[35\]](#page-6-0) was used to calculate the reactivity ratios of monomers in copolymers and the equation for this method can be written as

$$
\frac{x(y-1)}{\alpha y + x^2} = \frac{(r_1 + r_2/\alpha)x^2}{\alpha y + x^2} - \frac{r_2}{\alpha}
$$
\n(4)

where *x* and *y* are the molar ratios of monomers in feed and copolymer, respectively. The parameter,  $\alpha=\sqrt{\frac{\chi_{\min}\chi_{\max}}{y_{\min}y_{\max}}}$ , where  $\chi_{\min}$ ,  $\chi_{\max}$  are minimal and maximal molar ratios of monomers in feed;  $y_{\text{min}}$ ,  $y_{\text{max}}$ are minimal and maximal molar ratios of monomers in the copolymers. Using  $\eta = \frac{x(y-1)}{xy+x^2}$  and  $\xi = \frac{x^2}{xy+x^2}$  Eq. (4) can be written as

$$
\eta = (r_1 + r_2/\alpha)\xi - \frac{r_2}{\alpha} \tag{5}
$$

Thus the reactivity ratios  $r_1$  and  $r_2$  can be determined from the slope and intercepts of the plot of  $\eta$  against  $\xi$ . The Kelen–Tudos plots for SMMA, SEMA and SBMA are shown in Fig. S2 (see supplementary information). The monomer reactivity ratios for the copolymer SMMA are  $r_1(S)$  = 0.57 and  $r_2$  (MMA) = 0.54, for the copolymer SEMA are  $r_1$  (*S*) = 0.65 and  $r_2$  (EMA) = 0.32 and for the copolymer SBMA are  $r_1$  (*S*) = 0.52 and  $r_2$  (BMA) = 0.46, and the values are comparable with the values reported in literature [\[36\].](#page-6-0) The product of reactive ratios for each copolymer is lower than unity, indicating that all copolymers are random copolymers.

## *4.2. Thermal degradation*

Thermal degradation of the copolymers and homopolymers was studied using thermogravimetry at different heating rates of 5, 10, 15 and 20 $\degree$ C were used. The activation energies of the polymers at different conversions  $(\alpha)$  were calculated by using the Ozawa method [\[37\]](#page-7-0). In this method, the variation of conversion  $(\alpha)$  with heating rate is given by

$$
\log\left(\int_0^{\alpha} \frac{d\alpha}{g(\alpha)}\right) = \log\left(\frac{AE}{R}\right) - \log\varphi - 2.315 - 0.4567\left(\frac{E}{RT}\right) \tag{6}
$$

At fixed conversion, the activation energies are obtained from the slope of the plot of log  $\varphi$  against 1/*T*.

The Ozawa plots of homopolymers (PS, PMMA, PEMA and PBMA) and copolymers (SMMA-54, SEMA-56 and SBMA-54) are shown in [Figs. 1 and 2](#page-1-0), respectively. The normalized weight loss profiles of SMMA, SEMA and SBMA copolymers of different compositions are shown in Fig. S2 (see supplementary information). It can be inferred that the thermal stability of copolymers is higher than that of homopolymers (see Table S1 for activation energies). [Fig. 2](#page-2-0) depicts the effect of alkyl group substituent on the thermal stability of copolymers, and it follows the order SMMA > SEMA > SBMA.



Fig. 3. Variation of  $ln(Y)$  with sonication time for SMMA-54 (a) at 30 °C in different solvents and (b) in *o*-dichlorobenzene at different temperatures. Solid lines represent model fit.



Fig. 4. Variation of degradation rate coefficient of SMMA-54 with vapor pressure of the solvent.

#### *4.3. Differential scanning calorimetry analysis*

The glass transition temperatures of the copolymers were determined by using a DSC823<sup>e</sup> differential scanning calorimeter and the values are listed in Table S1 (see supplementary information). <span id="page-4-0"></span>It can be observed that the presence of styrene influenced the  $T_g$ of SEMA and SBMA copolymers and the effect was low for SMMA copolymers because the glass transition temperatures of their homo polymers are similar. The presence of styrene in the copolymer increased the  $T_g$  of SEMA and SBMA copolymers because of increased chain stiffness [\[38\]](#page-7-0), and  $T_g$  of SMMA decreased due to decreased polar–polar intermolecular interactions between ester groups [\[39\].](#page-7-0)



Fig. 5. Variation of ln(Y) with sonication time of (a) SMMA, (b) SEMA and (c) SBMA copolymers of different composition in *o*-dichlorobenzene at 30 °C. Solid lines represent model fit.

### <span id="page-5-0"></span>*4.4. Ultrasonic degradation*

#### *4.4.1. Effect of solvents*

The effect of solvents on the ultrasonic degradation of poly (styrene-*co*-alkyl methacrylate) copolymers was studied by investigating the degradation of SMMA-54 (54 mol% of MMA) at 30  $\degree$ C using different solvents. [Fig. 3](#page-3-0)a depicts the variation of ln(*Y*) with sonication time. The degradation rate coefficient in a particular solvent mainly depends upon the properties of solvent like vapor pressure and kinematic viscosity [\[5,7,9\]](#page-6-0) which primarily affect the cavitation capacity [\[40\]](#page-7-0) of the solvent. It was observed that the *k* value is a maximum in *o*-dichlorobenzene and minimum in benzene. The variation in rate coefficient for different solvents is mainly attributed to their cavitation capacity [\[10,40\]](#page-6-0) which governs the intensity of shock waves radiated from the collapsing cavity.

# *4.4.2. Effect of temperature*

The effect of temperature on degradation rate coefficient was studied on SMMA-54 copolymer in *o*-dichlorobenzene; the variation of ln(*Y*) with sonication time at different temperatures is illustrated in [Fig. 3](#page-3-0)b. It can be observed that the rate coefficient is higher at low temperature and decreases at higher temperature. At higher temperature, clearly the vapor pressure will be higher and so the vapor will enter the cavitation bubble, which leads to the cushioning effect [\[8,41\]](#page-6-0). The cushioning effect reduces the shock wave intensity and thus the rate of degradation. The increased viscosity of the solvent at lower temperatures increases rapid transmission of shock waves and favors the defragmentation of polymer chain at low strain rates [\[8,42\]](#page-6-0). [Fig. 4](#page-3-0) shows the effect of solvent vapor pressure on the degradation rate coefficient. The vapor pressure data was taken from standard handbook [\[43\].](#page-7-0)

# *4.4.3. Effect of alkyl group substituents*

[Fig. 5](#page-4-0) depicts the variation of ln(*Y*) with sonication time for various copolymers of different compositions in *o*-dichlorobenzene at 30 °C. The degradation rate coefficients ( $k \times 10^{-8})$  (mol g $^{-1}$  min $^{-1}$ ), obtained from the slope of the figures, of the homo polymers MMA, EMA and BMA are 5.8, 6.4 and 7.4, respectively, while that of copolymers SMMA-54, SEMA-56 and SBMA-54 are 5.0, 5.2 and 5.6, respectively. Fig. 6 shows that at any particular alkyl methacrylate composition, the ultrasonic degradation rate follows the order: SBMA > SEMA > SMMA. It indicates that the degradation rate increases with increase in the chain length of the alkyl methacrylate, which can be attributed to increased chain mobility. The increase of side chain in the polymer enhances the mobility and



Fig. 6. Variation of degradation rate coefficients of poly (styrene-*co*-alkyl methacrylate) copolymers with mol% styrene in *o*-dichlorobenzene at 30 °C.

further leads to increased scission in the main chain. A similar trend was observed in the thermal degradation of these copolymers [\(Fig. 2\)](#page-2-0), as discussed earlier.

#### *4.4.4. Effect of copolymer composition*

The dependence of the degradation rate coefficient on copolymer composition of poly (styrene-*co*-alkyl methacrylate) copolymers was investigated by conducting experiments over the entire range of composition for all copolymers at 30 °C in *o*-dichlorobenzene. The variation of ln(*Y*) with sonication time for different composition of SMMA, SEMA and SBMA copolymers is shown in [Fig. 5a–c](#page-4-0), respectively. It is clear that the model gives good fit to the experimental results. The rate coefficient for the ultrasonic degradation of the homopolymers and the copolymers are determined from the slope of the linearly regressed lines of [Fig. 5](#page-4-0).

Fig. 6 shows the variation of the rate coefficients with the copolymer composition for various copolymers. It can be observed that an increase in the styrene content in the copolymer has reduced the degradation coefficient of copolymers. This can be ascribed to increased mechanical properties of copolymers. Incorporation of vinyl aromatic monomer such as styrene in copolymer serves to improve the stability (mechanical and thermal) of polymer chains [\[44\].](#page-7-0) Further, the degradation rate coefficient is lower for some copolymers than either of the homo polymers, which indicates that the rate of degradation is not linear with styrene content. Similar trends were reported for mechanical properties of styrene alkyl methacrylate copolymers [\[45–47\]](#page-7-0). The mechanical properties of copolymers are primarily affected by the arrangement of two monomer units in the polymer backbone which influences the strength of polar-polar intermolecular interactions between monomers [\[48\]](#page-7-0). Fig. 7 represents the dependence of ultrasonic degradation coefficient, thermal activation energy, and tensile strength [\[46\]](#page-7-0) on mol% styrene in the SBMA copolymer.



Fig. 7. Variation of thermal activation energy, ultrasonic degradation rate coefficient and tensile strength of poly (styrene-*co*-butyl methacrylate) copolymers with mol% of BMA.

#### <span id="page-6-0"></span>*4.5. Comparison of ultrasonic and thermal degradation*

Previous studies have shown that the order of ultrasonic degradation of homopolymers of the alkyl acrylate series [27] follows the order, PBA < PEA < PMA i.e., the rate of degradation of poly (butyl acrylate) is slower than that of poly(methyl acrylate). This indicates that the degradation decreases with an increase in chain length of the side chain. However, the order of degradation of homopolymers of the alkyl methacrylate series [26] follows PBMA > PEMA > PMMA i.e., the degradation of poly(methyl methacrylate) is slower than that of poly(butyl methacrylate). This indicates that the degradation increases with an increase in chain length of side chains. Though the orders for the acryaltes and methacrylates seem to be anomalous, the orders are the same as that of thermal degradation of these polymers. Similarly, in this study, similar trends were observed in ultrasonic and thermal degradation of SMMA, SEMA and SBMA copolymers. Though the thermal degradation and mechanical properties of the copolymer are for the polymers in the solid state, the degradation rates of the copolymers in solution under ultrasonic exposure follow the same order [\(Fig. 7\)](#page-5-0). This study seems to indicate that the degradation rate of the copolymers in solution under ultrasound follows the same order as that of the mechanical strength of the polymers because ultrasonic degradation is similar to degradation under mechanical forces.

#### 5. Conclusions

In the present work the ultrasonic degradation of three different poly (styrene-*c*o-alkyl methacrylate) copolymers, viz. SMMA, SEMA and SBMA over entire range of composition was investigated. The reactivity ratios of the monomers were determined. A model based on continuous distribution kinetics was employed to obtain the degradation rate coefficients. The effect of solvent and temperature on the ultrasonic degradation of styrene–methyl methacrylate copolymer was studied and it is mainly attributed to vapor pressure of the solvent. The presence of styrene in the copolymers decreased the degradation rate coefficient of alkyl methacrylate copolymers mainly because of their improved mechanical properties. For any particular copolymer composition, the ultrasonic degradation rate follows the order SBMA > SE-MA > SMMA, and is attributed to increased main chain mobility which increases with the length of side chain. The thermal degradation of the copolymers was also investigated and the same degradation order as that of ultrasonic degradation was observed.

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#### Appendix A. Supplementary data

Supplementary data associated with this article can be found, in the online version, at [doi:10.1016/j.ultsonch.2010.02.003](http://dx.doi.org/10.1016/j.ultsonch.2010.02.003).

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